MEBS6000 Utility Services

Worked Example on Above and Underground Drainage Pipe Sizing (Updated – 7 December 2010)

Update – for corrected calculation in underground drain pipe sizing

Question

Consider a residential building having 20 storeys and each storey houses 8 flats. Each flat has a single bathroom (with a basin, a shower and a water closet) and a kitchen (with a sink and a washing machine).

Develop a draft schematic diagram for this building assuming two flats on each floor to share a vertical stack.

Solution

The discharge units (DU) for individual sanitary fitments in one flat are as follows:

Basin -0.3 L/s

Shower - 0.4 L/s

W.C. - 2.0 L/s (assume 9L cistern)

Sink – 1.3 L/s

Washing machine – 0.6 L/s

Total: 4.6 L/s (for one flat)

Total discharge units for one single stack = $4.6 \text{ L/s} \times 2 \times 20 \text{ storeys} = 184 \text{ DU}$ The design water flow is computed using K-factor

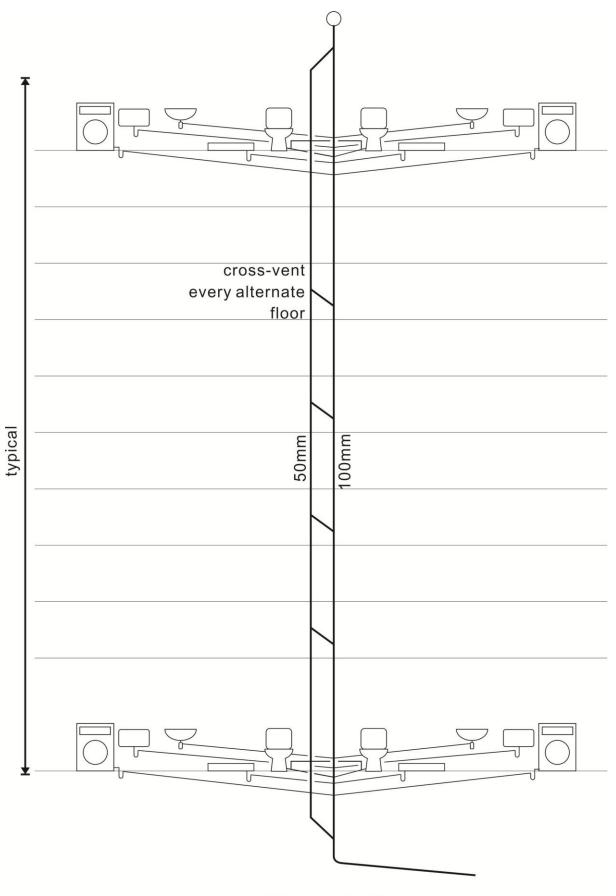
$$Q_{ww} = k\sqrt{\sum DU} = 0.5\sqrt{184} = 6.8 \text{ L/s}$$

With secondary ventilated discharge stack, 100 mm Ø stack + 50 mm Ø vent $\rightarrow 7.3 \text{ L/s}$ Thus, 100 mm Ø stack + 50 mm Ø vent are chosen

The draft schematic diagram for a single stack is shown.

Note:

- a) the venting for soil fitment
- b) cross vent between vent pipe and soil and waste stack every alternate floors
- c) vent pipe connecting the stack at the top and at the bottom of the vertical stack
- d) traps provided for all sanitary fitments



<u>Draft Schematic Diagram</u> <u>for a single stack</u>

Question

Consider a residential district with a population of 2500 residents. What will be the size of the main sewer pipe for the district?

<u>Solution</u>

The common design figure for residential discharge = 230L per person per day This figure is adopted for designing sewage treatment works.

When handling this data, the design discharge rate per hour is taken as:

½ of the daily discharge is made in a 6 hour period.

i.e. ½ of 230L is discharged into the sewage pipe work within 6 hours.

= $\frac{1}{2}$ x 230L / 6hr = 19.2L/hr for each resident

Thus, total discharge

 $= 19.2 \text{ L/hr} \times 2500 = 47917 \text{ L/hr} = 13.3 \text{ L/s} (0.0133 \text{ m}^3/\text{s})$

Consider half bore flow for the sewer pipe, and the design flow velocity = 1.5 m/s Let D = diameter of pipe

$$Q = \frac{\pi D^2}{4} \times \frac{1}{2} \times v$$

$$0.0133 = \frac{\pi D^2}{4} \times \frac{1}{2} \times 1.5$$

$$D = 0.15 \text{m}$$

Consider using 150mm pipe, the hydraulic mean depth (HMD or m_d) for ½ bore flow = D/4 (take note that only under ½ bore and full bore conditions that HMD = D/4, this ease up the difficulty in determining the HMD than other flow conditions)

i.e. m_d = 0.15/4 = 0.0375m

The inclination can be computed using Chezy Formula

$$v = c\sqrt{m_d \times i}$$

 $1.5 = 65\sqrt{0.0375 \times i}$ (Chezy Coefficient is usually taken as 65)

The inclination i = 0.0142 or 1 in 70 (this complies with the Buildings Regulations)

Thus the selected pipe size is Ø150mm and the inclination is 1 in 70.

It is necessary to find out the full bore carrying capacity (discharge) and the full bore flow velocity of the pipe selected so that we can compare the minimum flow against the full bore flow.

The full bore carrying capacity $Q_0 = 2 \times \frac{1}{2}$ bore capacity of pipe (see proportional table or chart for the relationship between ½ bore and full bore, i.e. at d/D = 0.5, $v/v_0 = 1.0$, $Q/Q_0 = 0.5$)

The full bore flow velocity v_o = ½ bore flow velocity (see proportional table or chart)

Thus, $Q_o = 0.0266 \text{m}^3/\text{s}$ and $v_o = 1.5 \text{m/s}$

It is necessary to check against minimum flow to ensure that self-cleansing velocity is met.

The minimum flow = 1/6 of design flow = 1/6 x 0.0133m³/s = 0.00222m³/s Thus, the proportional flow $\frac{Q}{Q_o} = \frac{0.00222}{0.0266} = 0.083$ (corrected)

From the proportional table or chart,

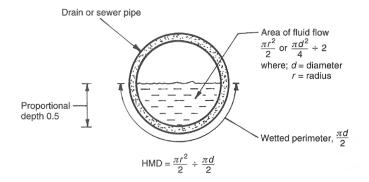
The proportional depth $\frac{d}{D}$ = 0.18 (corrected)

The proportional velocity $\frac{v}{v_0}$ = 0.67 (corrected)(note the slight deviation between the table and chart)

Thus, the velocity $v = 0.67v_0 = 0.67 \times 1.5 = 1.0$ m/s (> 0.75m/s self-cleansing velocity) (acceptable)

MEBS6000 Utility Services

Proportional Flow Chart Data for Circular Pipes laid to fall



| Proportional |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Depth | Velocity | Discharge | Depth | Velocity | Discharge | Depth | Velocity | Discharge |
| (d/D) | (v/v_0) | (Q/Q_0) | (d/D) | (v/v_0) | (Q/Q_0) | (d/D) | (v/v_0) | (Q/Q_0) |
| 0.01 | 0.163 | 0.0003 | 0.34 | 0.870 | 0.2608 | 0.67 | 1.080 | 0.7693 |
| 0.02 | 0.230 | 0.0011 | 0.35 | 0.880 | 0.2744 | 0.68 | 1.083 | 0.7843 |
| 0.03 | 0.281 | 0.0025 | 0.36 | 0.889 | 0.2883 | 0.69 | 1.086 | 0.7992 |
| 0.04 | 0.324 | 0.0043 | 0.37 | 0.899 | 0.3024 | 0.70 | 1.089 | 0.8139 |
| 0.05 | 0.361 | 0.0067 | 0.38 | 0.908 | 0.3166 | 0.71 | 1.091 | 0.8284 |
| 0.06 | 0.394 | 0.0097 | 0.39 | 0.917 | 0.3311 | 0.72 | 1.093 | 0.8426 |
| 0.07 | 0.425 | 0.0131 | 0.40 | 0.926 | 0.3458 | 0.73 | 1.095 | 0.8566 |
| 0.08 | 0.453 | 0.0170 | 0.41 | 0.934 | 0.3606 | 0.74 | 1.097 | 0.8703 |
| 0.09 | 0.479 | 0.0214 | 0.42 | 0.942 | 0.3756 | 0.75 | 1.099 | 0.8838 |
| 0.10 | 0.504 | 0.0262 | 0.43 | 0.950 | 0.3907 | 0.76 | 1.100 | 0.8969 |
| 0.11 | 0.527 | 0.0316 | 0.44 | 0.958 | 0.4060 | 0.77 | 1.101 | 0.9097 |
| 0.12 | 0.549 | 0.0373 | 0.45 | 0.966 | 0.4214 | 0.78 | 1.102 | 0.9222 |
| 0.13 | 0.570 | 0.0436 | 0.46 | 0.973 | 0.4369 | 0.79 | 1.103 | 0.9343 |
| 0.14 | 0.590 | 0.0502 | 0.47 | 0.980 | 0.4526 | 0.80 | 1.103 | 0.9460 |
| 0.15 | 0.610 | 0.0573 | 0.48 | 0.987 | 0.4683 | 0.81 | 1.103 | 0.9573 |
| 0.16 | 0.628 | 0.0648 | 0.49 | 0.994 | 0.4841 | 0.82 | 1.103 | 0.9682 |
| 0.17 | 0.645 | 0.0728 | 0.50 | 1.000 | 0.5000 | 0.83 | 1.103 | 0.9786 |
| 0.18 | 0.662 | 0.0811 | 0.51 | 1.006 | 0.5159 | 0.84 | 1.102 | 0.9884 |
| 0.19 | 0.679 | 0.0898 | 0.52 | 1.012 | 0.5319 | 0.85 | 1.101 | 0.9978 |
| 0.20 | 0.695 | 0.0989 | 0.53 | 1.018 | 0.5480 | 0.86 | 1.100 | 1.0066 |
| 0.21 | 0.710 | 0.1083 | 0.54 | 1.024 | 0.5640 | 0.87 | 1.099 | 1.0147 |
| 0.22 | 0.724 | 0.1182 | 0.55 | 1.029 | 0.5801 | 0.88 | 1.097 | 1.0222 |
| 0.23 | 0.739 | 0.1283 | 0.56 | 1.035 | 0.5962 | 0.89 | 1.095 | 1.0290 |
| 0.24 | 0.752 | 0.1389 | 0.57 | 1.040 | 0.6122 | 0.90 | 1.092 | 1.0350 |
| 0.25 | 0.766 | 0.1497 | 0.58 | 1.045 | 0.6283 | 0.91 | 1.089 | 1.0402 |
| 0.26 | 0.779 | 0.1609 | 0.59 | 1.049 | 0.6443 | 0.92 | 1.085 | 1.0444 |
| 0.27 | 0.791 | 0.1724 | 0.60 | 1.054 | 0.6602 | 0.93 | 1.081 | 1.0477 |
| 0.28 | 0.804 | 0.1842 | 0.61 | 1.058 | 0.6761 | 0.94 | 1.076 | 1.0497 |
| 0.29 | 0.815 | 0.1963 | 0.62 | 1.062 | 0.6919 | 0.95 | 1.070 | 1.0504 |
| 0.30 | 0.827 | 0.2086 | 0.63 | 1.066 | 0.7076 | 0.96 | 1.064 | 1.0495 |
| 0.31 | 0.838 | 0.2213 | 0.64 | 1.070 | 0.7232 | 0.97 | 1.056 | 1.0466 |
| 0.32 | 0.849 | 0.2342 | 0.65 | 1.074 | 0.7387 | 0.98 | 1.046 | 1.0410 |
| 0.33 | 0.860 | 0.2474 | 0.66 | 1.077 | 0.7541 | 0.99 | 1.033 | 1.0309 |

