TECHNICAL FEATURE

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Load Calculation Spreadsheets Quick Answers Without Relying on Rules of Thumb

By Steven F. Bruning, P.E., Fellow ASHRAE

ost HVAC design engineers use an array of sophisticated software calculation and modeling tools for load calculations and energy analysis. These tools offer almost total flexibility for the engineer to define physical arrangement, thermal parameters, operating schedules, internal loads and zoning. To achieve that flexibility, the input parameters are extensive and time consuming.

Especially in the early stages of a project, a large number of load assumptions must be made. Because the schedule is usually tight, using sophisticated modeling tools appropriate for detailed design can be problematic. Experienced designers often fall back on their historical assumptions of cfm/ft² or ft²/ton or

heating Btu/ft^2 to provide initial design and budget input.

An alternative approach to traditional rules of thumb is the use of simplified input spreadsheets. These have proven quick and easy to use for early concept and helpful in evaluating impact of assumptions vs. rules of thumb (which may not be valid with new trends in code and agency requirements).

Basic Load Calculation Spreadsheets

A new cooling load calculation technique was introduced by ASHRAE Technical Committee (TC) 4.1, *Load Calculation Data and Procedures*, in 2001 ASHRAE Handbook—Fundamentals. This method, radiant time series (RTS), effectively merged all previous "simplified" load calculation methods (TETD-TA, CLTD-CLF and transfer function). The RTS method and data were derived from fundamen-

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Figure 1 (above): Floor plan for example building used in the RTS calculation spread-sheet in *Figure 2*.

Figure 2 (right): Example RTS load calculation spreadsheet shows block load for a modular office building. The data took about 10 minutes to input.

tal heat balance calculations while maintaining simple concepts and componentby-component results. The new method was the result of years of ASHRAE research projects.

In 2003, TC 4.1 was asked by the ASHRAE Technical Activities Committee (umbrella group over all TCs) to develop a real-world building example load calculation for *ASHRAE Handbook*. The ASHRAE headquarters building, (two stories, 30,000 ft² [2787 m²]) was chosen as representative of many commercial office buildings.

To prepare that example, a series of demonstration RTS calculation spreadsheets were used. The spreadsheets were updated to incorporate results of additional ASHRAE research projects (new weather data, clear sky solar models, interior shading models, lighting heat to return air, etc.) for the 2009 Fundamentals. The 2013 Fundamentals example will be updated to incorporate the new addition and renovation of the ASHRAE headquarters building.

Those example RTS spreadsheets ("Radiant Time Series Method Load Calculation Spreadsheets" from the ASHRAE bookstore) are limited in function and are intended for educational purposes, but not to be used for full-blown commercial load calculations. While the procedures, techniques and data included in the spreadsheets are state-of-the-art, they would be impossibly cumbersome for use in typical projects involving hundreds or thousands of spaces. However, sometimes a quick analysis using the spreadsheets saves time, and the following are a few examples.

2009 ASHR	AE FUNDAM	ENTALS EX/	AMPLE-IP UN	IITS		rev 2009.05.	25	28-Nov-
	Burdell Engi	neering Asso	ciates				Geor	ge P. Burdell, P.
11N202	Modular Offi	ce Building	Long on the	La cara da la car				Baltimore, N
ROOM NO./	NAME:	100	Modular Of	fice Block Loa	bd			
	Length:	204	feet		-		Infiltration cfm	
	Width:	280	feet	Area	57120	sq. feet	Cooling:	Heating:
C	eiling Height	9	feet	Volume	514080	cubic feet	1000	2000
NTERNAL L	OADS:	1	Btuh/person:	Lighting,	Equipment,	Inside Desig	n Conditions:	
		# People:	Sensible:	watts:	watts:	Cooling:	DB, F	75
Over-ride	Room Input:	0	250	0	0		RH	50%
	Default	408	Latent:	62832	171360	Heating:	DB, F	72
	Use:	408	200	62832	171360	Outside Coo	ling Weather:	
EXPOSURE	S:	North	South	East	West	USA -	MD - BALTMORE BLT-W	VASHNGTN INTL -
Nomi	inal Azimuth:	-180	0	-90	90	Heating 99.6	%, F:	12.9
Act	tual Azimuth	-180	0	-90	90	Supply	Cooling, F	57
	Tilt	90	90	90	90	Air	Heating F	100
Type 1 \	Nall Area sf	5712	5712	3920	3920	Frame with F	FIES	
Type 21	Nall Area of	0	0	0	0	Frame with F	TIES	
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No. Type	2 Windows.	0	0	0	0	Dbl glazed, i	OW-E, DIDIZE	
No. Type	2 vvindows.	0	0	U D V V V V	U	DDI giz, Iow-	E, DINZ	
	Root Area, st.	28560	0%	= Root % to H	KA	0%	= Lights % to RA	
ROOM LOA	DS:	Peak Rm.Se	ens. Occurs:		Room	Ret. Air	Room	Roo
		Month:	7	Per Unit	Sensible	Sensible	Latent	Sensi
		Hour	18	Cooling	Cooling	Cooling	Cooling	Heatin
	OADS	nour.	No Poorte	Btub/core	Dtub	Buch	Buch	Treating De
INTERIVAL L	UAUS.	Deer	No. People:	Oturvpers 247	400 770	otun	Btun Dt COO	DI
		People:	408	241	100,776		81,600	
			watts:	Btuh/room sf	121720202			
	1.0.010	Lighting:	62,832	3.7	212,200			
	Lightii	ng % to RA:	0%	0.0		1949		
		Equipment:	171,360	10.2	580,832			
ENVELOPE	LOADS:							
		F	Roof Area,sf	Btuh/roof sf				
ROOF:	0.05	U factor	28,560	1.2	35,544			84,39
	R	oof % to RA:	0%			1949		
WALLS:		1	Vall Area.sf	Btuh/wall sf				
	Wall Type 1	Frame with	EIFS					
0.08	Il factor	North	5712	18	10.037			27.00
0.00	oractor	South	5712	2.2	12 299			27.00
		South	2020	10	7 464			27,00
		East	3920	1.0	7,101			10,5,
		West	3920	3.3	12,827			18,5
	Wall Type 2	Frame with I	EIFS	12.21.02				
0.08	U factor	North	0	0.0	8			
		South	0	0.0				
		East	0	0.0	2			2
		West	0	0.0				8
WINDOWS:		Wind	low Area.sf.	Btuh/win sf				
Wir	ndow Type 1:	Dbl glazed,	low-E. bronze					
1	sf/window	North	0	0.0	1			9
29%	SHGF(0)	South	0	0.0	140 A			
0.46	U factor	East	0	0.0				
7404	IAC	Wast	0	0.0	2			
1470	ndow Tuno 2	Dbl alt law	E broz	0.0				
VVII	offuinder	North	C, 0112	0.0				
0001	SUMINOW	Renth	0	0.0	*			
29%	ShGP(0)	South	0	0.0	5			
0.46	Utactor	East	0	0.0				
74%	IAC	West	0	0.0				-
INFILTRAT	ION LOADS		cfm	Btuh/cfm				
	Cooli	ng, Sensible:	1000	12.5	12,540			
	Co	oling, Latent:	1000	24.8			24,813	
		Heating:	2000	65.0				130.0
			1					
		8	00000000	TOTAL	084 206	-	106 412	305 40
		3	NOOM LOAL	TOTALS =	504,200	1 States	100,413	505,49
			COOL	ING CFM =	49,707	HEAT	ING CFM =	9,91
				CEMISE -	0.0			Canada Canada
				Crimor 4	0.9			
BLOCK LOA	ADS:	TOTAL ROC	M SENS+RA	+LATENT =	1,074,790		ROOM HTG:	305,4
Peak Block	Load Occurs	OUTSIDE A	IR: I	OA Sensible:	231,000		OA Heating:	812.6
Month:	7	OA cfm =	12500	OA Latent:	331,979		A	
11-2		CANLUTAT	50	UD to C. AL	107.005	-	THEATING	1 110 10
Hour:	15	FAN HEAT:	50	HP to S. Air.	127,305	10	HEATING, btuh=	1,110,12
	F	UMP HEAT	0	HP to CHW			Heating btuh/sf =	19.6
			NAM.			tons	sf/ton	Control of the second
				and the second second	4 765 074	4474	200	
				a new of the later and			100	
	TC	TAL BLOCK	COOLING	OAD, Dun -	1,100,014	1.41.1	000	

Quick Block Load Comparisons

At the earliest stage of a project, a quick block load calculation can be useful for defining mechanical spaces and cost modeling. This has been especially useful in the pricing phase of design-build competitions.

Figure 1 is a floor plan issued in an RFP. *Figure 2* is the RTS spreadsheet block load for this two-story building, which took about 10 minutes to input. What was unusual about this RFP is the building was to be constructed of modular units that could be disassembled and shipped to installations all over the

Fig	ur	e 3:
Blo	ck	load
for	a	secur

				No Wi	ndows			with 40% Windows						
	Location	supply		Cooling		Heating		supply		Cooling		Heating		
		cfm	cfm/gsf	tons	gsf/ton	1000/Btuh	btu/gsf	cfm	cfm/gsf	tons	gsf/ton	1000/Btuh	btu/gsf	
Figure 3.	Baltimore, MD	49,707	0.87	147	388	1,118	19.6	57,438	1.01	163	350	1,291	22.6	
	Bangkok, Thailand	50,730	0.89	175	326	108	1.9	59,060	1.03	192	297	125	2.2	
Block loads	Colorado Springs, CO	47,667	0.83	110	519	1,375	24.1	55,871	0.98	125	456	1,588	27.8	
for a secure	Darwin, Austrailia	50,210	0.88	170	337	161	2.8	57,979	1.02	184	311	186	3.3	
buildina in	El Paso, TX	51,009	0.89	125	456	935	16.4	60,038	1.05	144	397	1,079	18.9	
14 locations	Fairbanks, AK	46,759	0.82	96	597	2,181	38.2	53,384	0.93	110	517	2,519	44.1	
	Frankfurt, Germany	48,013	0.84	107	534	1,116	19.5	55,002	0.96	122	467	1,289	22.6	
	Honolulu, HI	49,479	0.87	143	401	204	3.6	56,698	0.99	158	362	236	4.1	
	Key West, FL	49,855	0.87	168	339	324	5.7	56,810	0.99	183	312	374	6.5	
	Kuwait City, Kuwait	54,416	0.95	151	377	617	10.8	66,594	1.17	175	327	712	12.5	
	Naples, Italy	49,431	0.87	144	398	689	12.1	57,138	1.00	160	357	795	13.9	
	Seattle, WA	47,324	0.83	101	567	899	15.7	53,268	0.93	114	501	1,038	18.2	
	Seoul, Korea	49,406	0.86	159	360	1,260	22.1	57,244	1.00	175	326	1,455	25.5	
	Tashkent, Uzbekistan	50,773	0.89	127	452	1,076	18.8	59,948	1.05	145	393	1,243	21.8	



Figure 4 (left): Typical floor plan for military barracks project. Figure 5 (right): Site plan for military barracks project.

world. What impact would different climates have on the heating and cooling loads?

Design weather data for the 5,564 worldwide locations included in the 2009 ASHRAE Handbook-Fundamentals CD+ is embedded in the RTS spreadsheet and selected with a simple drop-down menu. So, in another 20 minutes, block loads were identified for 14 locations (Figure 3). This particular building is a secure facility with no windows, so variations due to climate were mostly due to outside air conditions.

For curiosity's sake, the same block loads were run for a building with 40% glass (Figure 3). This was quick because the spreadsheet includes the tabulated fenestration solar heat gain coefficient data from Chapter 15 of the 2009 ASHRAE Handbook—Fundamentals selected in a simple drop-down box.

Cooling supply Orientation cfm/gsf tons gsf/ton cfm 0 14,553 0.55 52.4 508 15 503 14.816 0.56 52.9 30 15.149 0.57 53.4 498 45 15.539 0.58 495 53.7 60 15,839 0.60 54.1 492 75 16,018 0.60 54.2 491 90 16,068 0.60 54.2 491

Figure 6: This shows the difference orientation makes in load for the military barracks project.

Another useful quick evaluation is multiple identical buildings with different orientations on the same site. While the ASHRAE spreadsheet only includes four orientations (NSEW), it does include an orientation correction factor that effectively allows quick "rotation" of those orientations.

Figure 4 is a typical floor plan, and Figure 5 is a site plan for a multiple barracks project. How much difference did the various orientations make in the building block load? Figure 6 includes the results. In this case, this 10-minute exercise confirmed impact on peak due to orientation for this location and particular building type.

Using Spreadsheets for Zone Load Model

While the RTS spreadsheets are useful for simple block load calculations, with a little front-end effort, the ASHRAE RTS Example spreadsheets can provide a tool useful in evaluating

peak loads for each perimeter zone vs. block loads for each floor and the building as a whole. Again, at the early concept stage of a project, this is useful, particularly for designbuild competitions and space allocation input.

Many buildings boil down to mostly rectangular floor plans of one or more stories. In most cases, cooling and heating loads are bro-

ken into interior and perimeter zones. Using the ASHRAE RTS Example worksheets, a simple model with eight perimeter zones and one interior zone per floor can be assembled. A master input worksheet links dimensional data to the individual zone worksheets, and their results link back to a single-page summary. For buildings that fit within a simple rectangular concept, this provides a tool



Figure 7: Floor plan from a design-build project.

to quickly assess zone and overall cooling and heating loads.

As an example, Figure 7 is a floor plan from a design-build RFP with perimeter, corner and interior zones overlaid. Figure 8 is the front-end input required for the spreadsheet and the results are in Figure 9. When the impact of increasing glazing from 20% to 50% was questioned, a single input was changed and total supply air increased 8% and total cooling 4.5% to 333 tons (1171 kW), a quick way to accurately respond to a client's questions.

Rules of Thumb

Most engineers develop a feel for building cooling and heating capacity over years of practice, forming rules of thumb: "400/ft² per ton," "1 cfm/ft²," and "25 Btu/h·ft²" heating. These rules have been

TS COOLING	LOAD CAL	CULATIONS	5		BLOCK ZC	A Novemb	er 28, 2011	
009 A SHRAE F	UNDAMEN	TALS EXAM	PLE-IP UN	IITS		Page:	1	
ENTIFICATIO	N:	De	esign Firm:	Burdell En	gineering			
		Project	Engineer:	George P.	Burdell, P			
		Proj	ect Name:	Headquart	ters Additio	on		
		Projec	t Location:	USA - GA	COLUMBL	JS METROPOL	ITAN ARPT - 5%	
		Projec	t Number:	09N240				
Floor F	Plate Size:	INTERNA	L LOADS			WALL		
N side, ft	250	250 sf per person:		Input	Actual "U" :	ctual "U" : 0.05		
E side, ft.	134	People:	100	A	bsorbtance:	0.45		
	degrees			Brick, R-5	Insulation B	oard, Sheathing	, R-11 Batt Insulation,	Gyp Board
Rotation:	0	W	atts per sf:		Wall #:	13		
# Stories	4	Lighting:	1.1			ROOF	A	HU FAN HEAT
Perimeter	Depth, ft	% to RA:	26%	Input .	Actual "U" :	0.04		hp/1000 cfm
Zone:	15			A	bsorbtance:	0.45		1.0
Unconditi	oned Core:	W	atts per sf:		% to RA:	30%		
% Interior	15%	Plug Load:	3	Membrane,	Sheathing,	R-15 Insulation	Board, Metal Deck	
Floor to	Height, ft	-			Roof #:	11		
Floor:	14	OUTSIDE AIF		R		WINDOW	BUILDING	G PUMP HEAT
Ceiling:	9	cfm/pers:	10		SHGC (0) =	22%		hp/ton
Percent of	Below Clg:	+ cfm/sf	0.1	Input	Actual "U" :	0.39		0.1
% Glazing:	20%							

Figure 8: The front-end input required for the RTS spreadsheet for the design-build project.

RTS COOLING LOAD CALC	CULATIONS		users a	BLOCK ZON	November 28, 20					
2009 A SHRAE FUNDAMEN	TALS EXAM	PLE-IP UI	NITS	1	ev 2011.11	1.13	Page:	1		
IDENTIFICATION:	Des	sign Firm:	Burdell En	gineering A	ssociates					
	Project	Engineer:	George P.	George P. Burdell, P.E.						
	Proje	ect Name:	Headquart	ers Addition						
	Project	Location:	USA - GA -	COLUMBUS	METROP	OLITAN AR	PT - 5%			
	Project	Number:	09N240							
		Peak	Peak	Cooling	Cooling	Room				
ZONE	Area,sf	Month	Hour	cfm	cfm/sf	heating				
North Perimeter-Top floor	3,300	7	15	3,104	0.94	19,728				
South Perimeter- Top Floor	3,300	9	14	3,301	1.00	19,728				
East Perimeter-Top Floor	1,560	7	15	1,507	0.97	9,326				
West Perimeter-Top Floor	1,560	7	17	1,673	1.07	9,326				
NW corner-Top Floor	225	7	17	267	1.19	2,268				
NE Corner-Top Floor	225	7	15	245	1.09	2,268				
SE Corner-Top Floor	225	8	14	254	1.13	2,268				
SW Corner-Top Floor	225	8	16	271	1.21	2,268				
Interior-Top Floor	19,448	7	16	15,950	0.82	36,484				
		Sum of	Zone cfm =	26,571			OA cfm	Ton		
Top Floor AHU	30,068	7	16	26,376	0.88	103,665	6014	81.		
A CALENDARY CONTRACTOR				99%		413,906	=Htg w OA	367		
						14	=Htg btu/sf	sf/to		
North Perimeter-Typ floor	3,300	7	16	2,881	0.87	13,537				
South Perimeter- Typ Floor	3,300	10	14	3,166	0.96	13,537				
East Perimeter-Typ Floor	1,560	7	10	1,469	0.94	6,399				
West Perimeter-Typ Floor	1,560	7	17	1,579	1.01	6,399				
NW corner-Typ Floor	225	7	17	254	1.13	1,846				
NE Corner-Typ Floor	225	7	11	230	1.02	1,846				
SE Corner-Typ Floor	225	8	14	240	1.07	1,846				
SW Corner-Typ Floor	225	8	16	257	1.14	1,846				
Interior-Typ Floor	19,448	1	18	14,766	0.76	-				
	Construction of the	Sum of	Zone cfm =	24,841			OA cfm	Ton		
Typ Floor AHU	30,068	7	17	24,405	0.81	47,257	6014	76.		
				98%		357,499	=Htg w OA	393		
						12	=Htg btu/sf	sf/to		
							OA cfm	Ton		
Building Block Load	120.272	7	16	99,477	0.83	245,436	24054	318.		
						1,486,403	=Htg w OA	378		
						12	=Htg btu/sf	sf/to		

Figure 9: RTS spreadsheet results for design-build project.

fairly common for office buildings in some parts of the country. Two ASHRAE Standards: 90.1 and 62.1, have had a tremendous impact on the building industry over the past 30 years. But what kind of impact have they had on our rules of thumb? *Figure 10* is a compilation of criteria from Standards 90.1 and 62.1 over the years that impact peak heating and cooling loads. Likewise, plug load trends went up during the 1980s and 1990s, but have begun to reduce due to more

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	Window	Window	Window	Wall	Roof	People	OA	OA	Lights	Plug	supply	Cooling	Heating
Time Frame	%	U	SHGC	U	υ	sf/pers	cfm/pers	cfm/sf	w/sf	w/sf	cfm/sf	sf/ton	Btuh/sf
Common 1980	51%	0.8	0.6	0.150	0.100	100	15	0	3	1	1.07	311	19
1989	51%	0.45	0.45	0.130	0.072	143	20	0	1.57	2	0.98	380	14
1999	39%	0.45	0.29	0.124	0.063	143	20	0	1.3	2	0.81	436	13
2010	39%	0.65	0.24	0.084	0.048	200	5	0.06	0.9	1	0.53	671	11

Figure 10: A look back at criteria from Standards 90.1 and 62.1 that impact peak heating and cooling loads.

efficient desktop and laptop computers and use of LCD monitors. The RTS spreadsheets were used for block loads for a common suburban office building (five stories, 25,000 ft² [2323 m²] per floor in Atlanta) with these parameters with results in *Figure 10*. The impact on overall block loads and resulting rules of thumb has been significant over the past 30 years.

is especially true in early concept stages for architectural planning input, sizing of equipment spaces, shafts, etc. Simple block loads are also especially helpful in developing cost models in competition phases of design-build projects or for evaluating parameters such as location and orientation.

Conclusions

Today's complex buildings require sophisticated load calculation software to account for the myriad variations in exposures, construction, zoning, load densities and occupancy.

However, there are cases where a simple load calculation spreadsheet can be a time-saving, useful tool. This Likewise, comparative studies of impact of trends due to standards (such as 90.1 and 62.1) or assumptions (plug loads) can be readily evaluated with a simple spreadsheet without investing the time and energy required for a fullblown commercial software calculation. The spreadsheets can illustrate impacts of individual components relative to the overall total loads, sometimes lost with more complex tools.



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