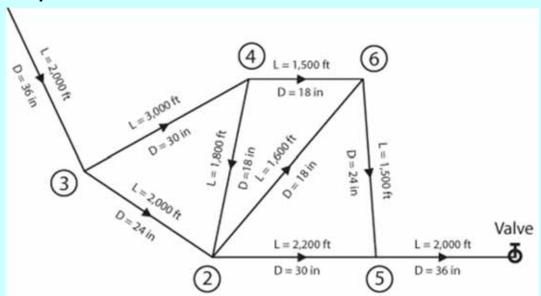
#### MEBS6008 Environmental Services II

http://www.mech.hku.hk/bse/MEBS6008/



### Fluid Network Analysis II



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#### **Contents**

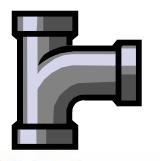


Pipe Systems and Design

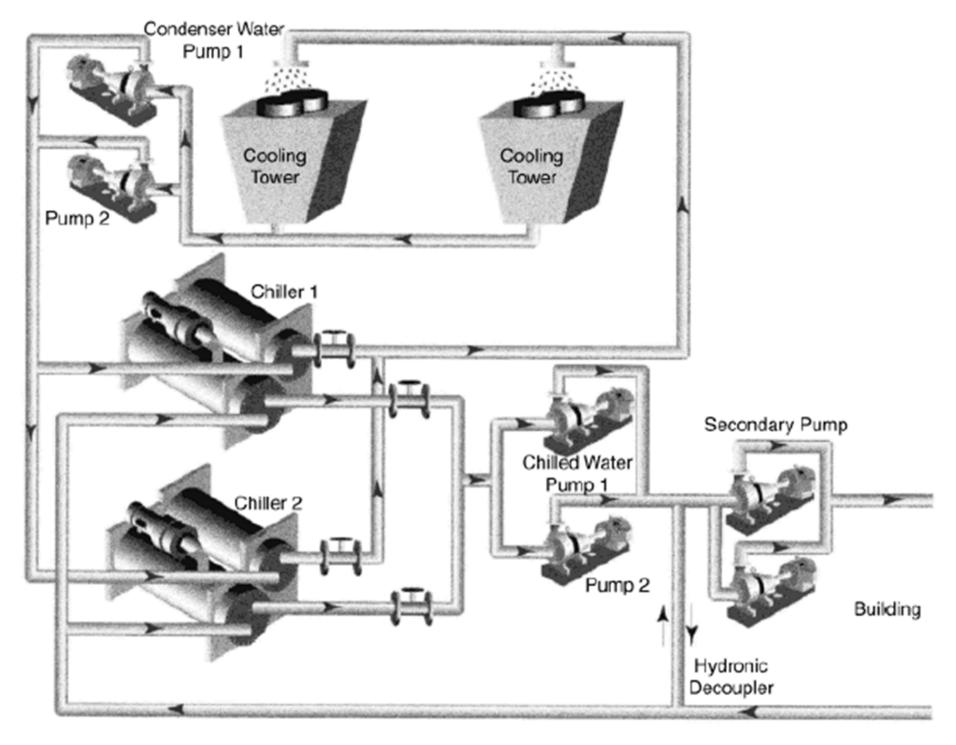
Pipe Network Analysis

Water Systems in HVAC





- Common types of HVAC piping systems
  - Chilled water (CHW) system
  - Condenser water (CW) system
  - Sea water system
  - Hot water supply system
  - Steam pipes, gas pipes
- Similar systems in other building services
  - Water supply & distribution (plumbing)



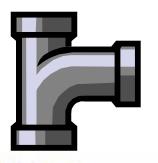
[Source: Kreider, K. F. (ed.), 2001. Handbook of Heating, Ventilation, and Air Conditioning, CRC Press, Boca Raton, FL.]





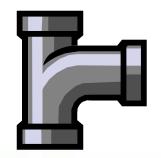
- Two major concerns:
  - Size the pipe (e.g. from charts & tables)
  - Determine the flow-pressure relationship
    - To analyse the system, e.g. to find out pump pressure
    - By using manual or computer-based methods
- Calculations for pipelines or pipe networks
  - Can be very complicated for branches & loops
  - Basic parameters: pipe diameter, length, friction factor, roughness, velocity, pressure drop





- Pipe network analysis
  - Physical features are known
  - Solution process try to determine flow & pressure at every node
- Pipe network design
  - Variables are unknown
  - Try to solve & select pipe diameters, pumps, valves, etc.





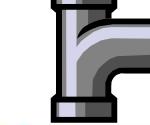
- Basic equations
  - <u>Darcy-Weisbach Equation</u> (for fully developed flows of all Newtonian fluids)

$$\Delta p = f\left(\frac{L}{D}\right)\left(\frac{\rho V^2}{2g}\right)$$
 or  $\Delta h = f\left(\frac{L}{D}\right)\left(\frac{V^2}{2g}\right)$ 

Colebrook-White Equation (for transition region):

$$\frac{1}{\sqrt{f}} = 1.14 + 2\log(D/\varepsilon) - 2\log\left[1 + \frac{9.3}{\operatorname{Re}(\varepsilon/D)\sqrt{f}}\right]$$

• \* The equation is implicit in *f* (appears on both sides), so iterations are required to solve for *f*.



# Pipe Systems and Design

- Basic equations (cont'd)
  - Hazen-Williams Equation (alternative to Darcy-Weisbach formula; empirical)

$$\Delta p = 6.819L \left(\frac{V}{C}\right)^{1.852} \left(\frac{1}{D}\right)^{1.167} (\rho g)$$

• C = roughness factor (typically, C = 150 for plastic or copper pipe, C = 140 for new steel pipe, C < 100 for badly corroded or very rough pipe)



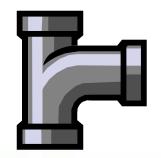


- Basic equations (cont'd)
  - Exponential formula:
    - The previous equations (Darcy-Weisbach or Hazen-Williams) can be expressed by an exponential form to generalise the theory

$$\Delta h = KQ^n$$

- Q = volume flow rate; K, n = coefficient & exponential
- Values for the coefficient and *n* change, depending on which equation is used





- Valve and fitting losses
  - May be greater than pipe friction alone

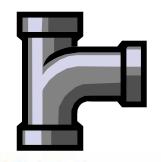
$$\Delta p = K_L \rho \left(\frac{V^2}{2}\right)$$
 or  $\Delta h = K_L \left(\frac{V^2}{2g}\right)$ 

- $K_L = loss$  coefficient (K factor) of pipe fittings
  - Geometry and size dependent
  - May be expressed as equivalent lengths of straight pipe
- Valve coefficient  $(A_v)$ :
  - Volume flow rate  $Q = A_v \sqrt{\Delta p / \rho}$

Table 2.5 Loss Coefficients for Fittings

| Fitting   | $K_L$                     |
|---|---------------------------|
| Globe valve, fully open                           | 10.0                      |
| Angle valve, fully open                           | 5.0                       |
| Butterfly valve, fully open                       | 0.4                       |
| Gate valve, fully open 3/4 open 1/2 open 1/4 open | 0.2<br>1.0<br>5.6<br>17.0 |
| Check valve, swing type, fully open               | 2.3                       |
| Check valve, lift type, fully open                | 12.0                      |
| Check valve, ball type, fully open                | 70.0                      |
| Foot valve, fully open                            | 15.0                      |
| Elbow, 45°  | 0.4                       |
| Long radius elbow, 90°                            | 0.6                       |
| Medium radius elbow, 90°                          | 0.8                       |
| Short radius (standard) elbow, 90°                | 0.9                       |
| Close return bend, 180°                           | 2.2                       |
| Pipe entrance, rounded, r/D < 0.16                | 0.1                       |
| Pipe entrance, square-edged                       | 0.5                       |
| Pipe entrance, re-entrant                         | 0.8                       |





- Practical design issues
  - Select a pipe size for desired total flow rate and available or allowable pressure drop, e.g.
    - Often assume 2.5 m / 100 m pipe length
    - Velocity limit 1.2 m/s for pipe < 50 mm dia., pressure drop limit 400 Pa/m for pipe > 50 mm dia.
  - Rule of thumb for practical design:
    - Assume design pipe length is 1.5 to 2.0 times actual to account for fitting losses; after pipe diameter is selected, then evaluate the influence of each fitting
  - Other considerations: e.g. noise & water hammer

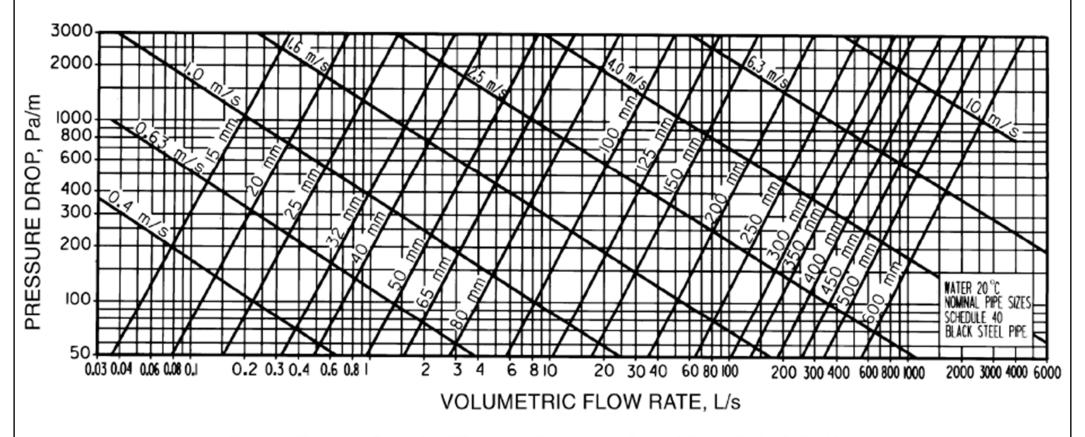


Fig. 4 Friction Loss for Water in Commercial Steel Pipe (Schedule 40)

(Source: ASHRAE Handbook Fundamentals 2005, Chp. 36)

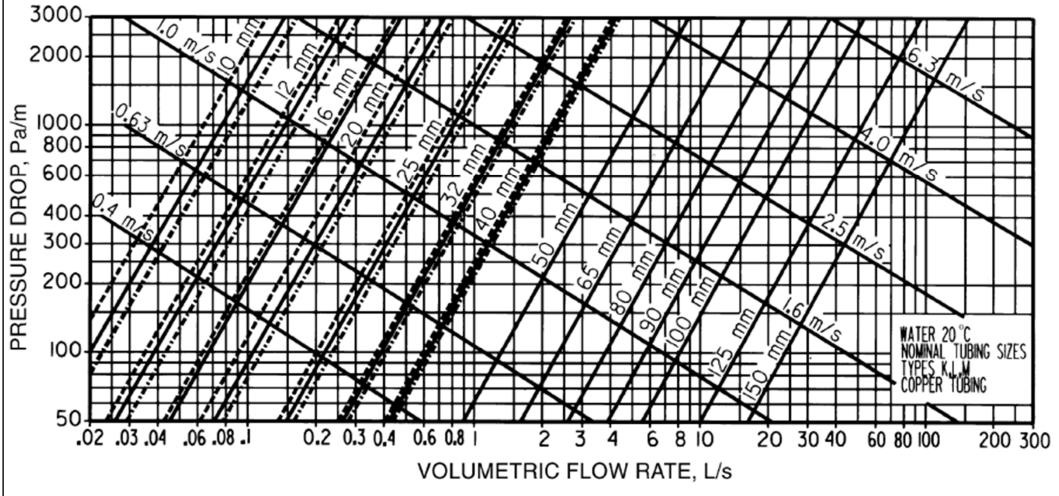


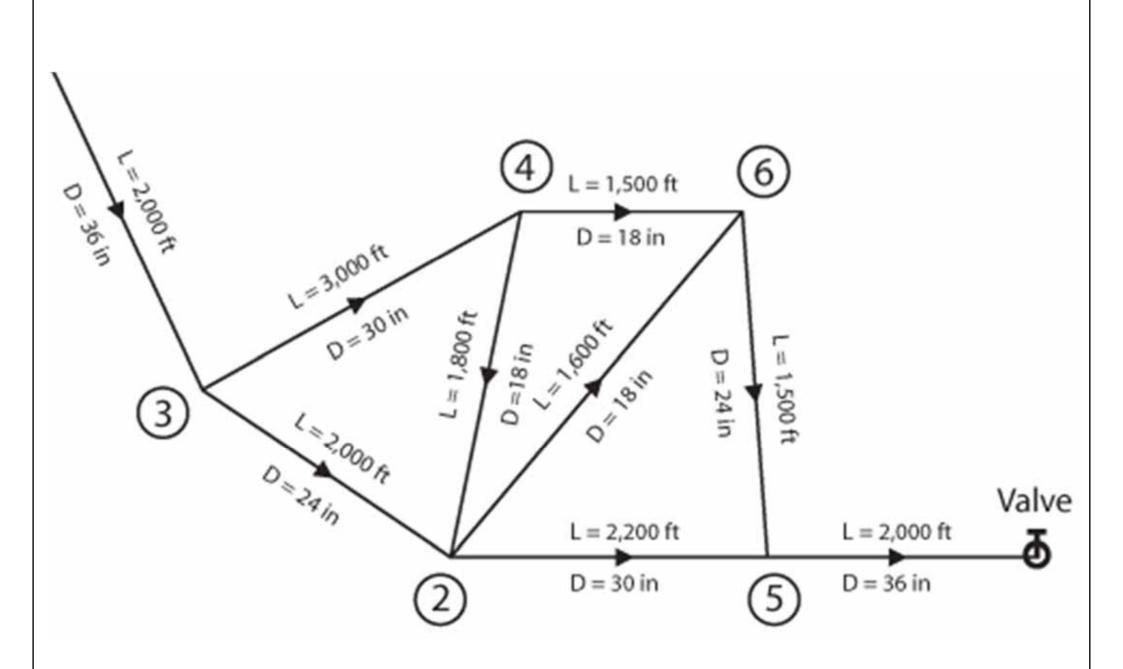
Fig. 5 Friction Loss for Water in Copper Tubing (Types K, L, M)

(Source: ASHRAE Handbook Fundamentals 2005, Chp. 36)





- Often a complex mathematical problem
  - Solving entire set of non-linear equations
  - Large networks are usually analysed by computers
- Basis of the computer solutions
  - Basic principles of fluid mechanics
  - Suitable equations that embody them
  - Interrelate the pipe discharge & pressure at each node of the network

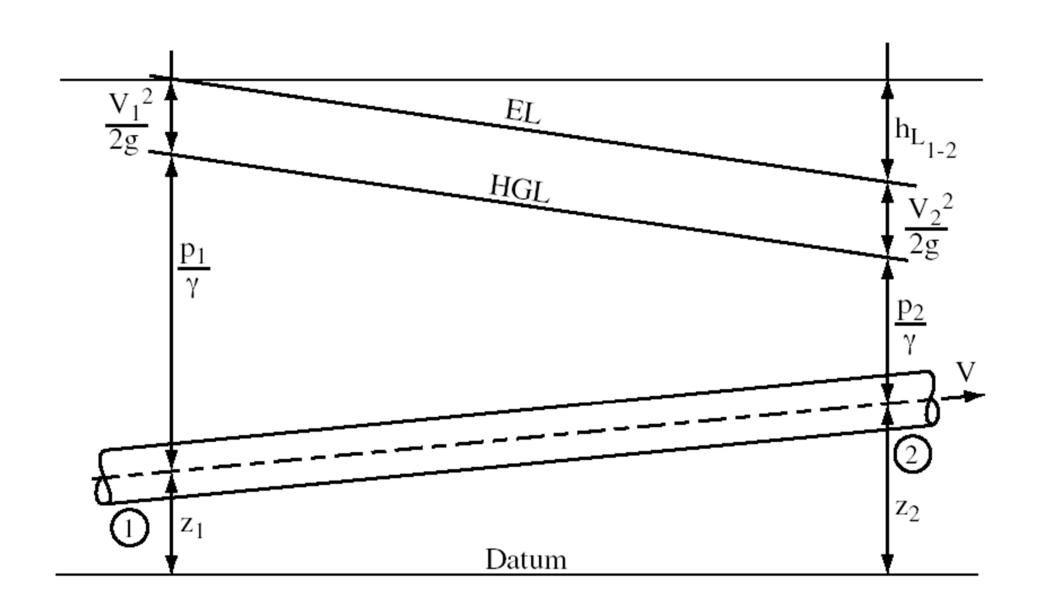


Pipe network analysis





- Basic principles of fluid mechanics
  - 1) Conservation of mass (continuity principle)
  - 2) Work-energy principle (Darcy-Weisbach or Hazen-Williams)
  - 3) Fluid friction & energy dissipation
- The task is to
  - Describe the hydraulic system accurately and efficiently by means of equations
  - Solve these simultaneous equations effectively



Energy Line (EL) and Hydraulic Grade Line (HGL)





- Methods to solve steady flow problem in a pipe network
  - Hardy Cross method
    - Adapted from structural engg.
    - Oldest systematic method; suited for hand computations
    - Convergence problems for large systems
  - Newton method
    - Linear algebra matrix operations
    - Perform iterative set of calculations (using computers)



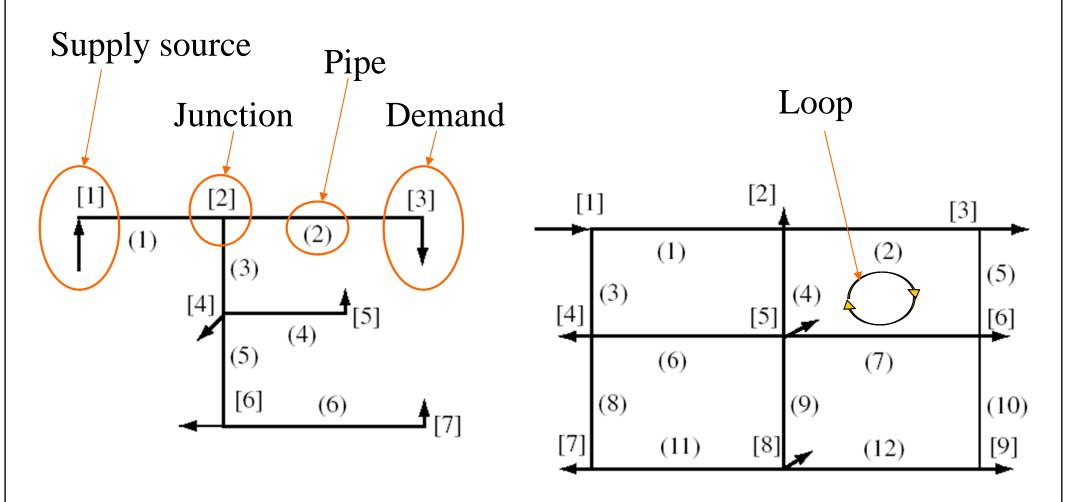


- Define an appropriate pipe system
  - Decide what features are important & to retain
    - No hard rules; requires much insight & judgment
  - Determine which demands should be specified
    - Analysis for a range of system demands
  - For large systems, require some "skeletonization"
    - Not all pipes or nodes are included in the analysis
    - Some may be lumped at a single node
  - After studying the entire system, more detailed analysis may be done within a building or area





- Basic relations between network elements
  - Junction Continuity Equations
    - Summing volume flows at each junction (or node)
  - Energy Loop Equations
    - Summing initial energy within a network loop with the friction losses within that loop
  - Basic parameters:
    - NP = number of pipes
    - NJ = number of junctions
    - NL = number of loops
  - Branched system and looped system



**Figure 4.1** (a) A small branched system. 6 pipes, 7 nodes

(b) A small looped system. 12 pipes, 9 nodes





- Equations for steady flow in networks
  - *Q-equations* (pipe charges are the unknowns)
  - *H-equations* (heads are the unknowns)
  - <u>AQ-equations</u> (corrective discharges are the unknowns)
  - When the equations are established, may use Newton method to solve them
    - Linear algebra matrix operations
    - Determine Jacobian matrix
    - Iterative procedure to calculate desired discharges





- Q-equations (assume flow as unknowns)
  - Based on continuity
    - Flow into a junction = Flow out of the junction

$$QJ_{j} - \sum Q_{i} = 0 \quad QJ_{j} = \text{flow out (demand)}$$

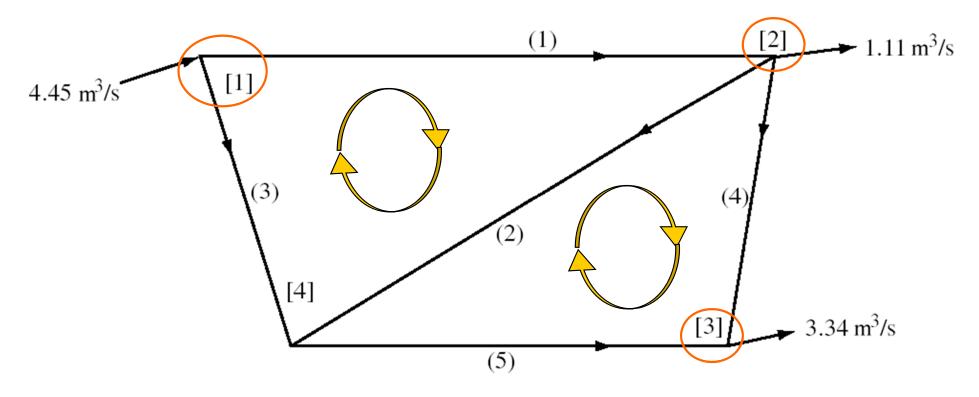
$$Q_{i} = \text{flow in from pipe } i$$

- Based on work-energy principles
  - Sum of the head loss around each loop is zero

$$\sum_{i} h_{fi} = \sum_{i} K_{i} Q_{i}^{n} = 0 \qquad h_{fi} = \text{head loss}$$

$$K_{i}, n = \text{coefficients}$$

#### Example of *Q*-equations for a simple network



Node [1]: 
$$Q_1 + Q_3 - 4.45 = 0$$

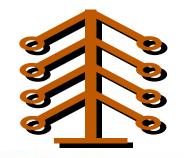
Node [2]: 
$$-Q_1 + Q_2 + Q_4 + 1.11 = 0$$

Node [3]: 
$$-Q_4 - Q_5 + 3.34 = 0$$

Loop 1-2-3: 
$$K_1Q_1^n + K_2Q_2^n - K_3Q_3^n = 0$$

Loop 4-5-2: 
$$K_4Q_4^n - K_5Q_5^n - K_2Q_2^n = 0$$





- <u>*H*-equations</u> (assume head as unknowns)
  - Solve the exponential equation for the flow

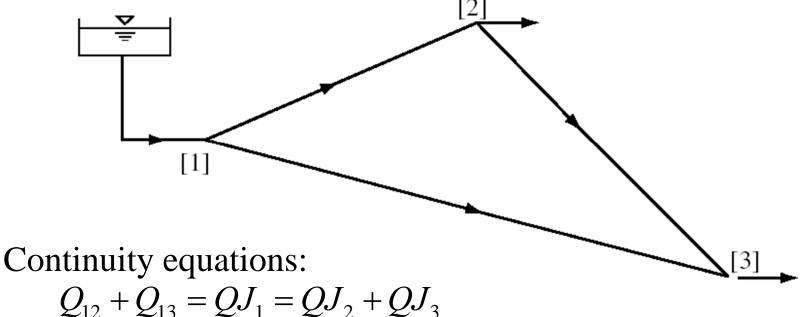
$$Q_{ij} = (h_{fij} / K_{ij})^{1/n_{ij}} = [(H_i - H_j) / K_{ij})]^{1/n_{ij}}$$

- Subscript ij = for the pipe from node i to node j
- Substitute the above into junction continuity equ.

$$QJ_{j} - \sum \{ [(H_{i} - H_{j})/K_{ij})]^{1/n_{ij}} \}_{in}$$

$$+ \sum \{ [(H_{i} - H_{j})/K_{ij})]^{1/n_{ij}} \}_{out} = 0$$

#### Example of *H*-equations for a simple network



$$Q_{12} + Q_{13} = QJ_1 = QJ_2 + QJ_3$$
  
 $Q_{21} + Q_{23} = -QJ_2$  (or  $-Q_{12} + Q_{23} = -QJ_2$ )

*H*-equations (by substituting the *Q* above):

$$\left[\frac{H_1 - H_2}{K_{12}}\right]^{1/n_{12}} + \left[\frac{H_1 - H_3}{K_{13}}\right]^{1/n_{13}} = QJ_2 + QJ_3$$

$$- \left[\frac{H_1 - H_2}{K_{12}}\right]^{1/n_{12}} + \left[\frac{H_2 - H_3}{K_{23}}\right]^{1/n_{23}} = -QJ_2$$

# Pipe Network Analysis



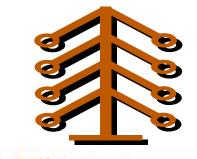
- <u>AQ</u>-equations (corrective flows as unknowns)
  - To obtain these equations, replace the flow in energy loop equations by an initial  $Q_{0i}$ , plus the sum of all initially unknown corrective flow

$$Q_i = Q_{0i} + \sum \Delta Q_k$$

Energy equation becomes

$$\sum K_i \{Q_{0i} + \sum \Delta Q_k\}^{n_i} = 0$$

• Nos. of equations can be reduced, but the equations are nonlinear & contain many terms



## Pipe Network Analysis

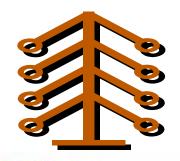
- Solving the network equations
  - Newton iterative formula:

$$\{x\}^{(m+1)} = \{x\}^{(m)} - [D]^{-1} \{F\}^{(m)}$$

- $\{x\}$  = entire column vector of unknowns
- $\{F\}$  = entire column vector of equations
- $[D]^{-1}$  = inverse of matrix [D], the Jacobian

$$\{x\} = \begin{cases} x_1 \\ x_2 \\ \vdots \\ x_n \end{cases} \qquad \{F\} = \begin{cases} F_1 \\ F_2 \\ \vdots \\ F_n \end{cases} \qquad [D] = \begin{bmatrix} \frac{\partial F_1}{\partial x_1} & \frac{\partial F_1}{\partial x_2} & \cdots & \frac{\partial F_1}{\partial x_n} \\ \frac{\partial F_2}{\partial x_1} & \frac{\partial F_2}{\partial x_2} & \cdots & \frac{\partial F_2}{\partial x_n} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial F_n}{\partial x_1} & \frac{\partial F_n}{\partial x_2} & \cdots & \frac{\partial F_n}{\partial x_n} \end{bmatrix}$$

# Pipe Network Analysis



- Solving the network equations (cont'd)
  - Newton method solves a system of nonlinear equations by iteratively solving a system of linear equations. The iterative formula is:

$$\{x\}^{(m+1)} = \{x\}^{(m)} - \{z\}$$

- $\{z\}$  = solution vector, solved by  $[D]\{z\} = \{F\}$
- The solution is developed by using a multidimensional Taylor series expansion to evaluate the individual equation

#### An example of simple pipe network analysis (using MathCAD)

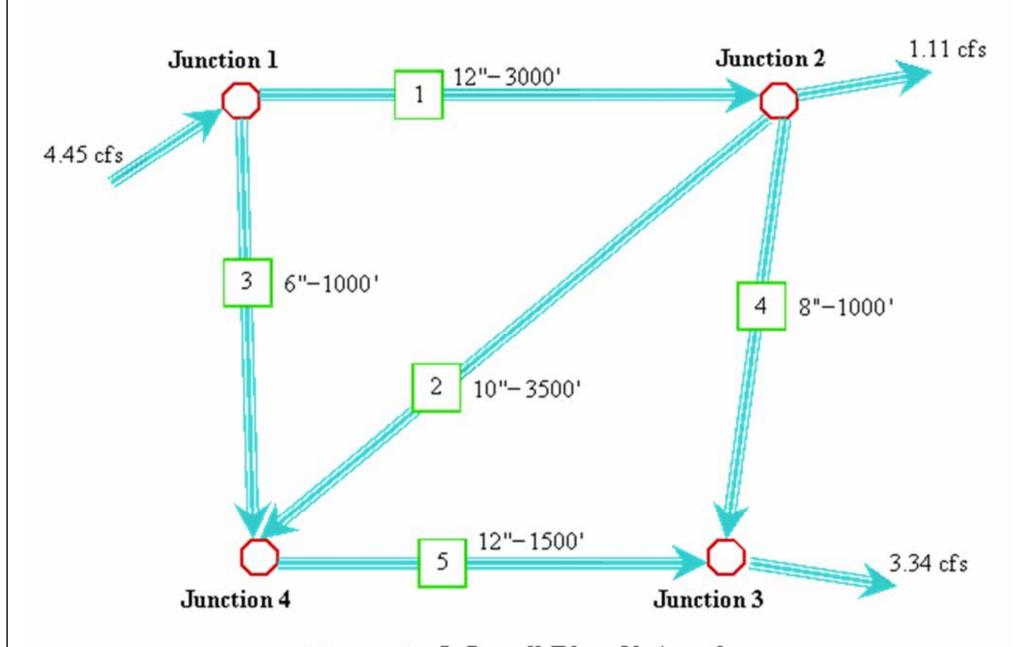
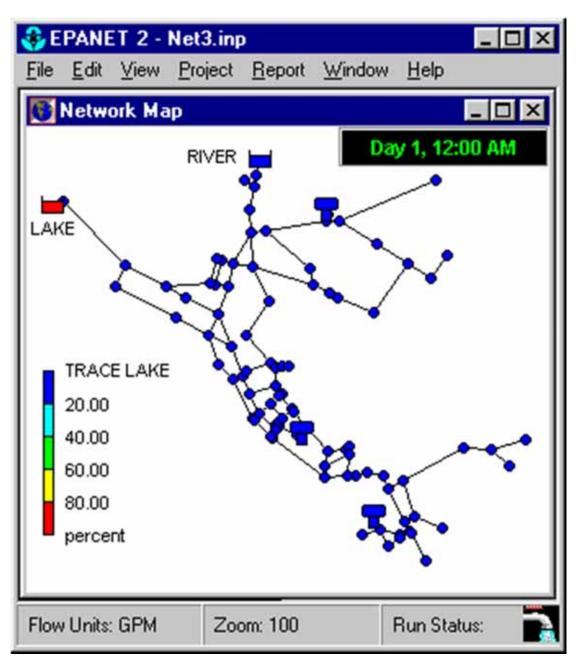


Figure 1: A Small Pipe Network





- Computer solutions to networks
  - Implement using equation solver package e.g.
     MathCAD, or computer programs e.g. FORTRAN
  - Other pipe analysis software are available, e.g. EPANet (for water supply & distribution)
    - http://www.epa.gov/nrmrl/wswrd/dw/epanet.html
  - Simple demon. of piping simulation software:
    - http://www.vcity.ou.edu/demoModules/piping/home.ht
       m



EPANET 2.0 interface

(Source: http://www.epa.gov/nrmrl/wswrd/dw/epanet.html)



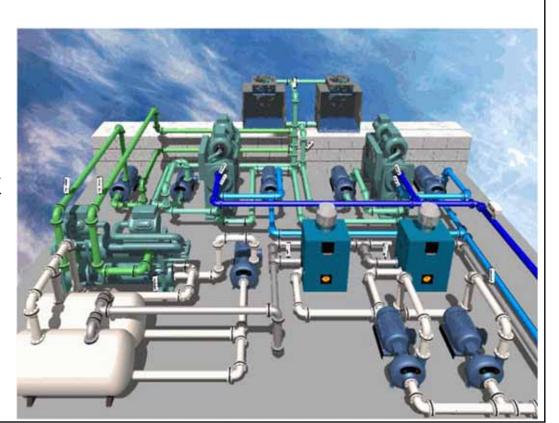


- After the analysis is done, the next step is to verify by measurements in actual system (network verification) & identify deficiencies
  - Such as for designing water supply systems
- Application to HVAC systems
  - At present, large network analysis is not common in HVAC, except district cooling system (DCS)
  - But the technique can be applied to studies of water systems, air systems and building infiltration



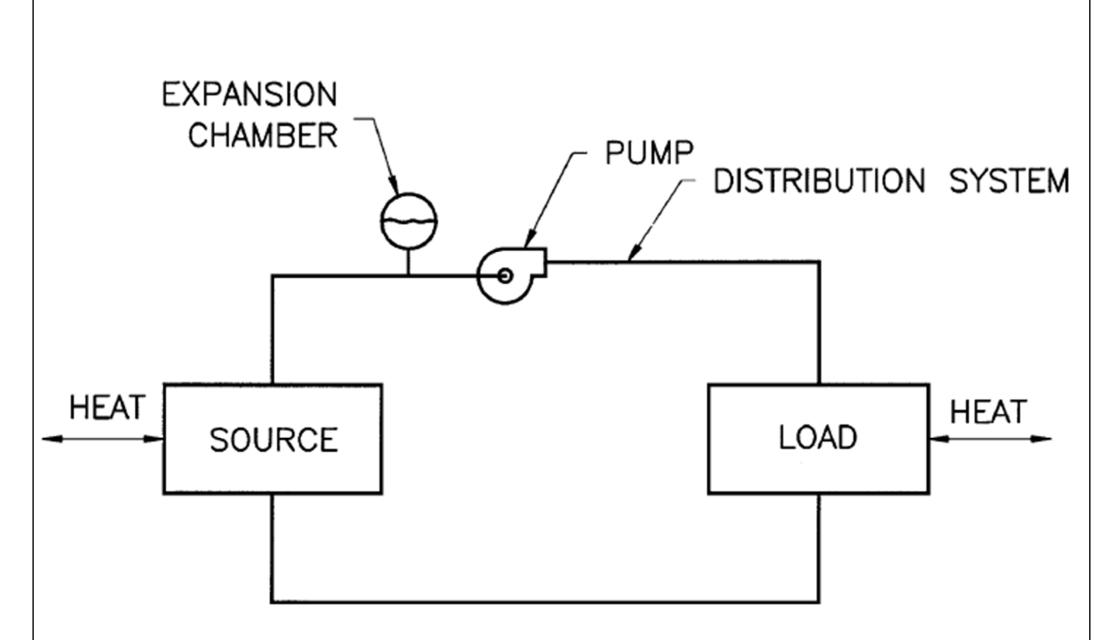


- HVAC water systems can be classified by
  - Operating temperature
  - Flow generation
  - Pressurization
  - Piping arrangement
  - Pumping arrangement

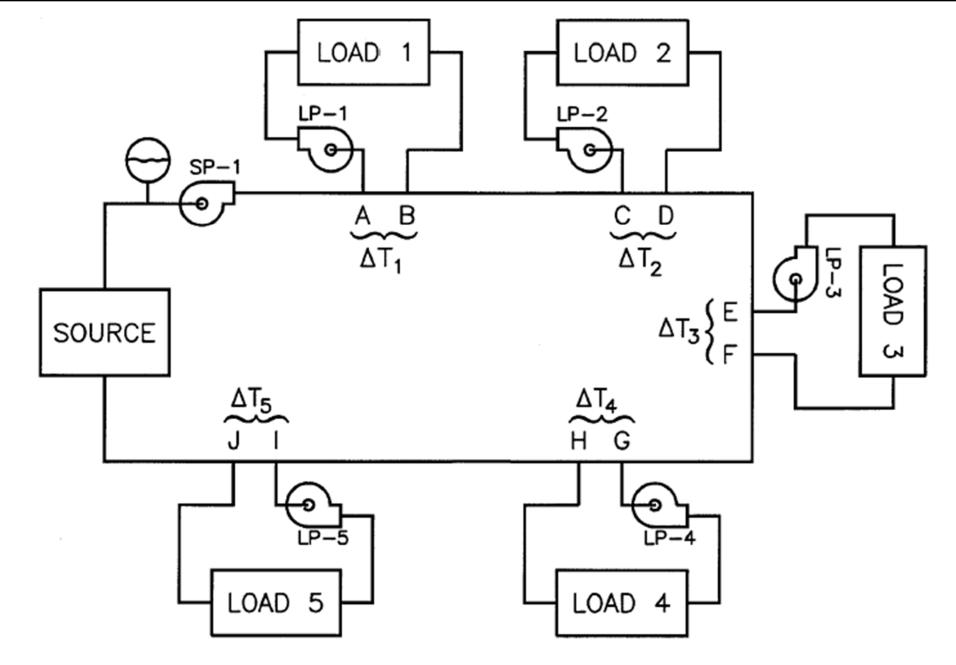


## Water Systems in HVAC

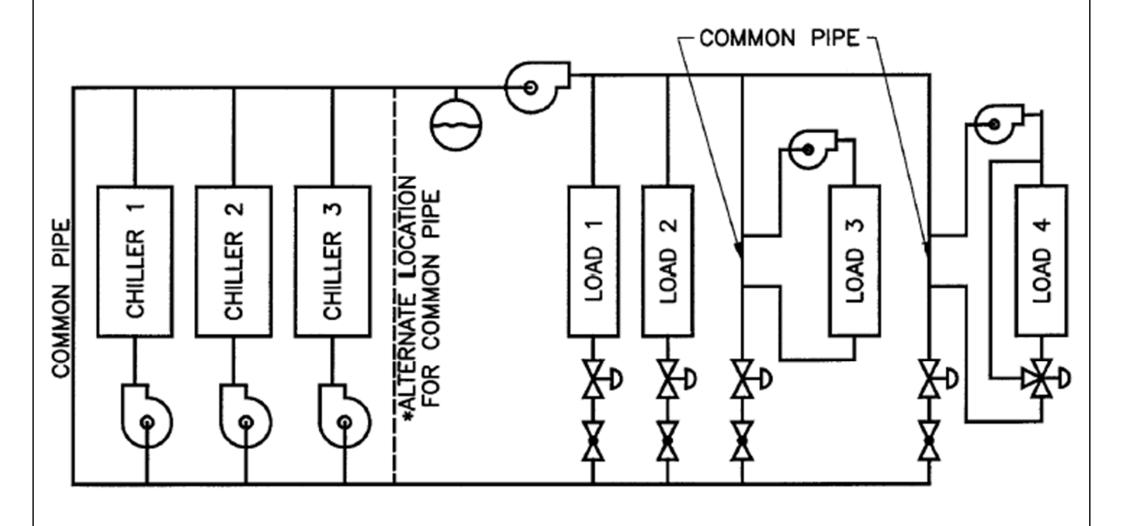
- Open water systems, e.g. using cooling tower
- Closed water systems
  - Chilled water (CHW) system [4-13 °C, 825 kPa]
  - Condenser water (CW) system
  - Dual temperature water system
  - Low temp. water (LTW) system [Max. 120 °C, < 1100 kPa]
  - Medium temp. water (MTW) system [120-125 °C, < 1100 kPa]</li>
  - High temp. water (HTW) system [> 175 °C, > 2070 kPa]
- Once-through system, e.g. sea water system



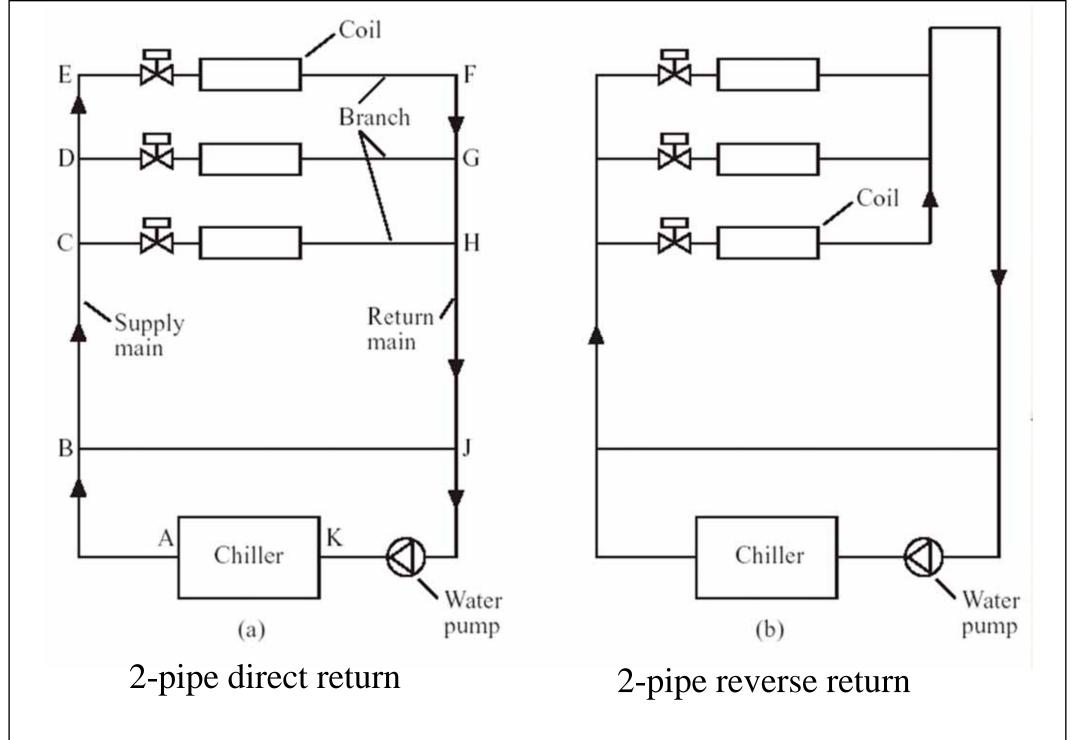
Basic components of water (hydronic) system

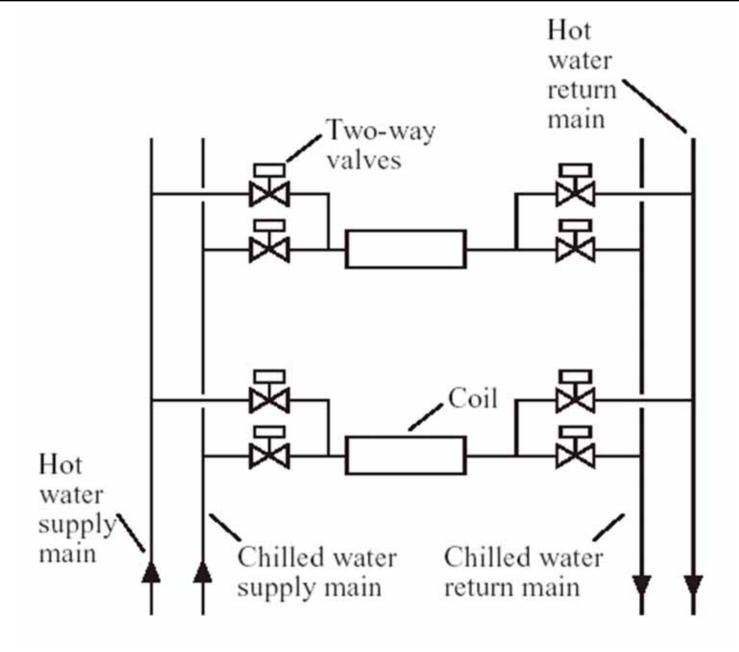


Series circuit with load pumps



Multiple chiller variable flow chilled water system





4-pipe system (dual temperature)



- Heat transfer in water systems
  - Terminal units/devices that convey heat from/to water for heating/cooling
  - Common heat exchangers
    - Water-to-air finned coil
    - Water-to-water
  - Heating load devices, e.g. radiators
  - Cooling load devices, e.g. fan coil units (FCU)

#### Calculate Heat Transferred to or from Water:

$$q_w = 1000 \dot{m} c_p \Delta t$$

#### where

 $q_w$  = heat transfer rate to or from water, W

m = mass flow rate of water, kg/s

 $c_p$  = specific heat of water, kJ/(kg·K)

 $\Delta t$  = water temperature increase or decrease across unit, K

 $1000 = \text{constant to change kJ in } c_p \text{ to J}$ 

$$q_w = \rho_w c_p Q_w \Delta t$$

where

 $Q_w$  = water flow rate, L/s

 $\rho_w$  = density of water, kg/m<sup>3</sup>





- Design issues
  - Design water temperature
  - Flow rate
  - Piping layout
  - Pump selection
  - Terminal unit selection
  - Control method



- Design principles
  - Constant flow? Variable flow? Intermittent flow?
  - Direct return piping or reverse return piping
  - Direct return riser & reverse zone piping
- Design factors
  - Pump speed controls
  - Pressure distribution
  - System balancing
  - Thermal expansion & joints (or loops)



- Piping materials
  - Chilled water: black & galvanized steel
  - Hot water: black steel, hard copper
  - Condenser water: black steel, galvanized ductile iron, PVC
- Flow rate measurements
  - Venturi, nozzle & orifice flowmeters
  - Variable area flowmeters (rotameters)
  - Turbine flowmeters



- Other design considerations
  - Makeup water (from city water or wells)
  - Safety relief valves (for pressurised systems)
  - Air elimination (e.g. by air separator/vent)
  - Drain (at low points) & shutoff (for isolation)
  - Balance fittings (allow balancing of sub-circuits)
  - Strainers (remove dirt)
  - Insulation (reduce heat loss & condensation)
  - Condensate drains (to drainage system or recover)



- Practical design process (see reference)
  - See "*Practical Guide to HVAC Building Services Calculations*" - water flow distribution systems: overview of system design process
    - W1 Pipe sizing general
    - W2 Pipe sizing straight length
    - W3 Pipe sizing pressure drop across fittings
    - W4 System resistance for pipework index run
    - W5 Pump sizing
    - W6 Water system pressurisation